



Status of the ITER FW&S Design

Conceptual Design

May 11, 2005

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Presented at PFC Technology Meeting
At PPPL



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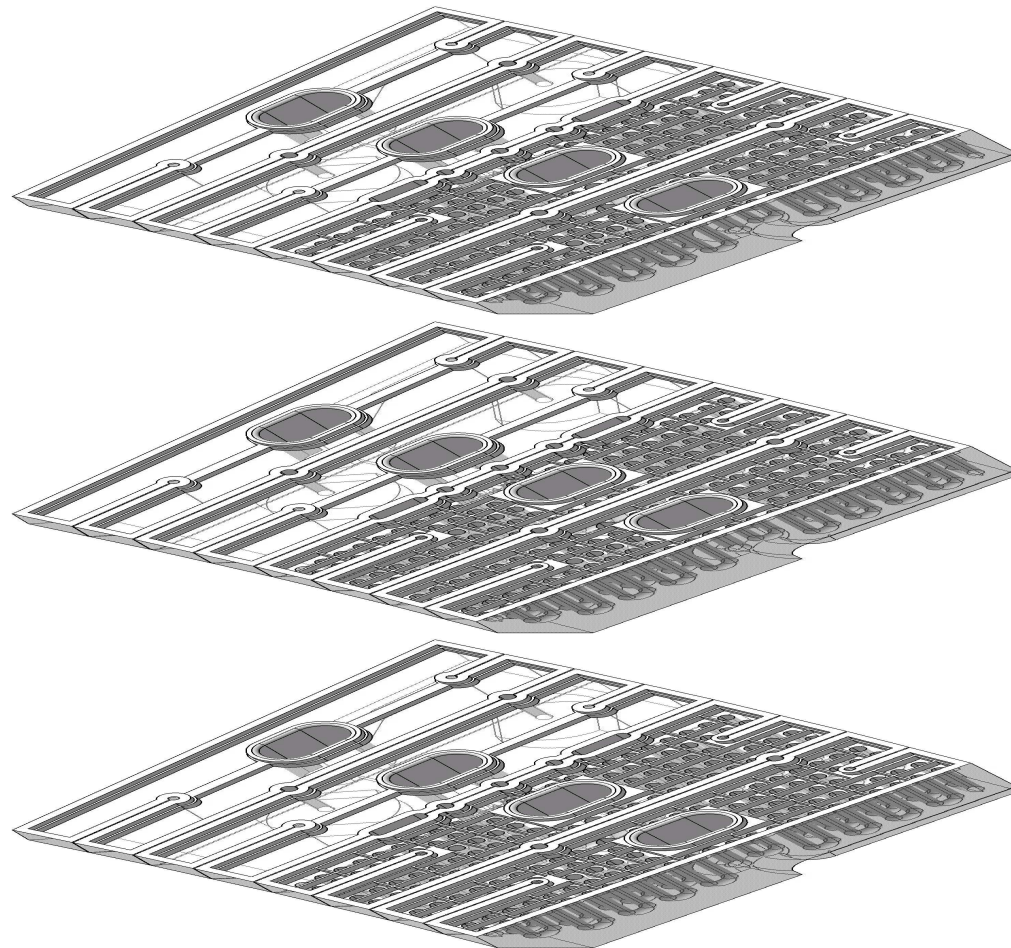


Outline

- **Shield Module**
 - Physical layout
 - Thermal Analysis
 - Electromagnetic Analysis
- **First Wall**
 - Physical layout
 - Thermal Analysis
 - Electromagnetic Analysis
- **Issues to be resolved**

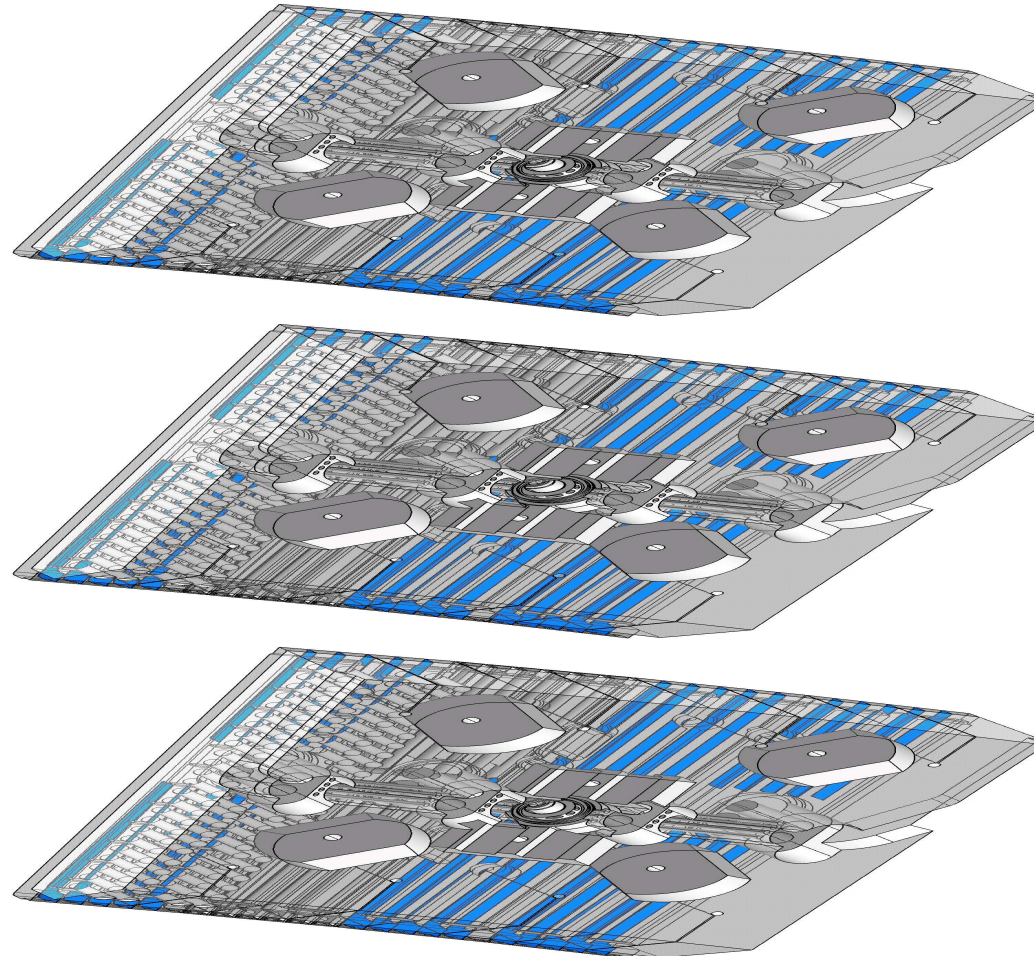


Shield-layout





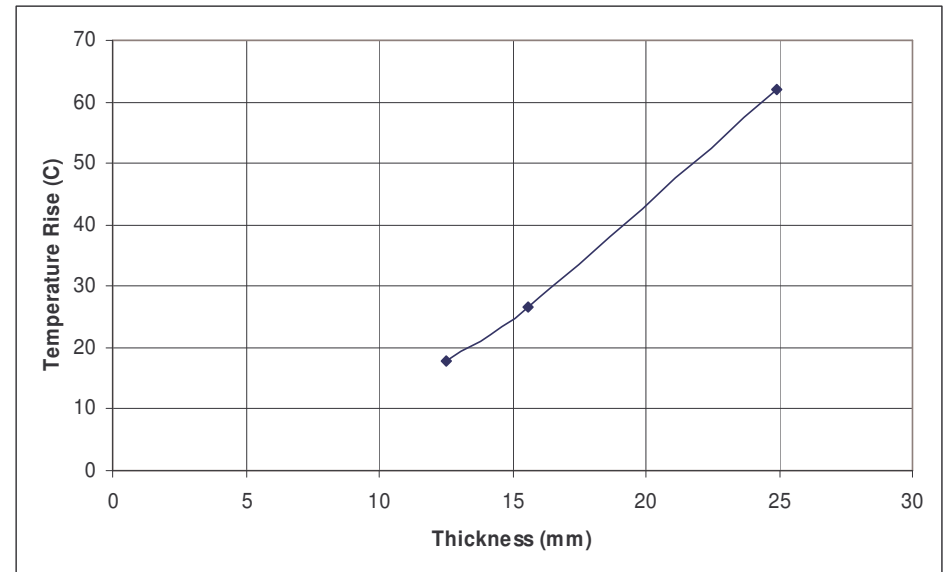
Shield-layout





Shield Thermal Analysis

- Temperature rise due to nuclear heating has been calculated with 3.6 W/cm^3
- The temperature rise in the stainless is only due to nuclear heat
- A ΔT of about 16 C over 4 mm is sufficient to cause stresses of about yield in 316 LN Steel





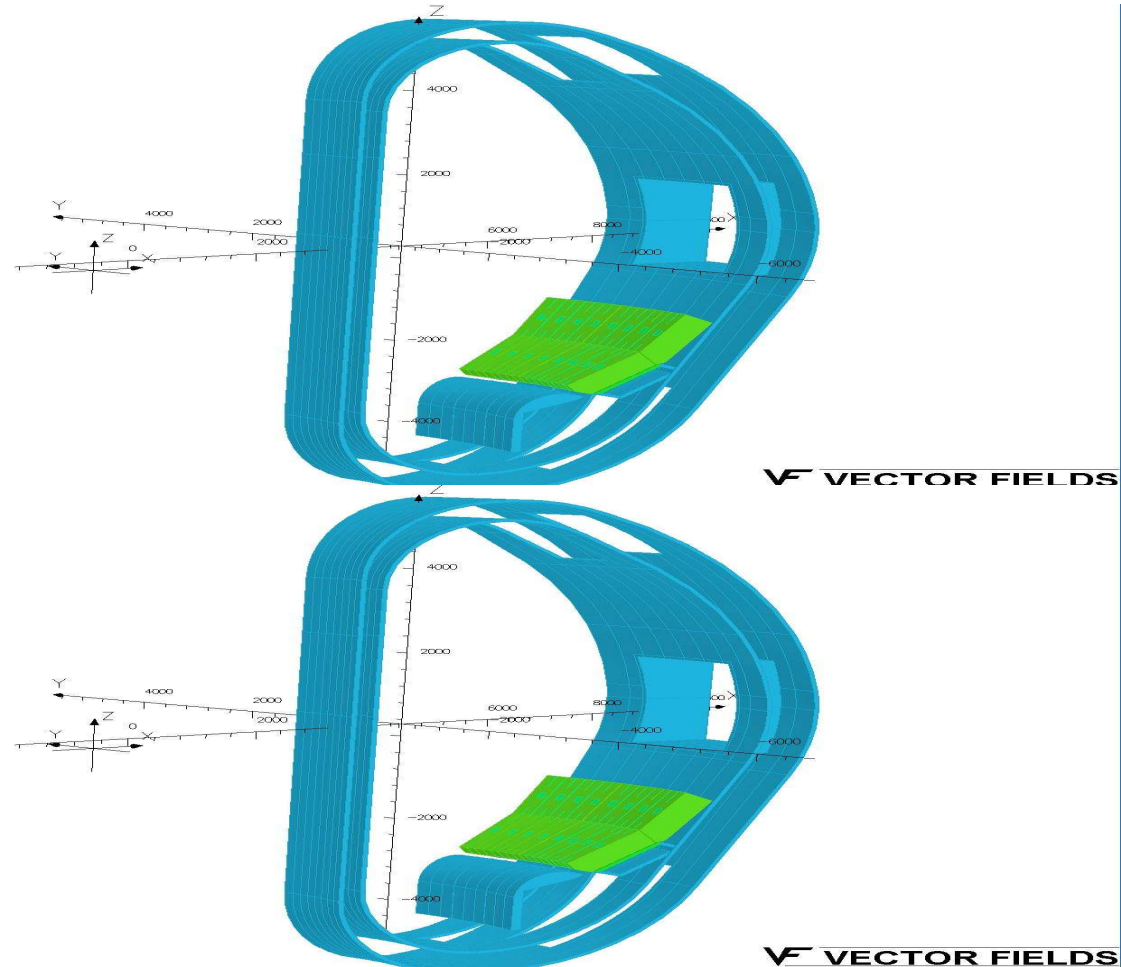
Shield EM Analysis

- A complete 20 degree sector of the vacuum vessel, ports, lower triangular support, module 18 and 17, and the divertor was constructed in OPERA. PF coils were included. TF simulated by a single wire.
- Two disruption cases were provided by IT
 - An 18 ms exponential current decay vertical disruption
 - A 40 ms linear decay VDE



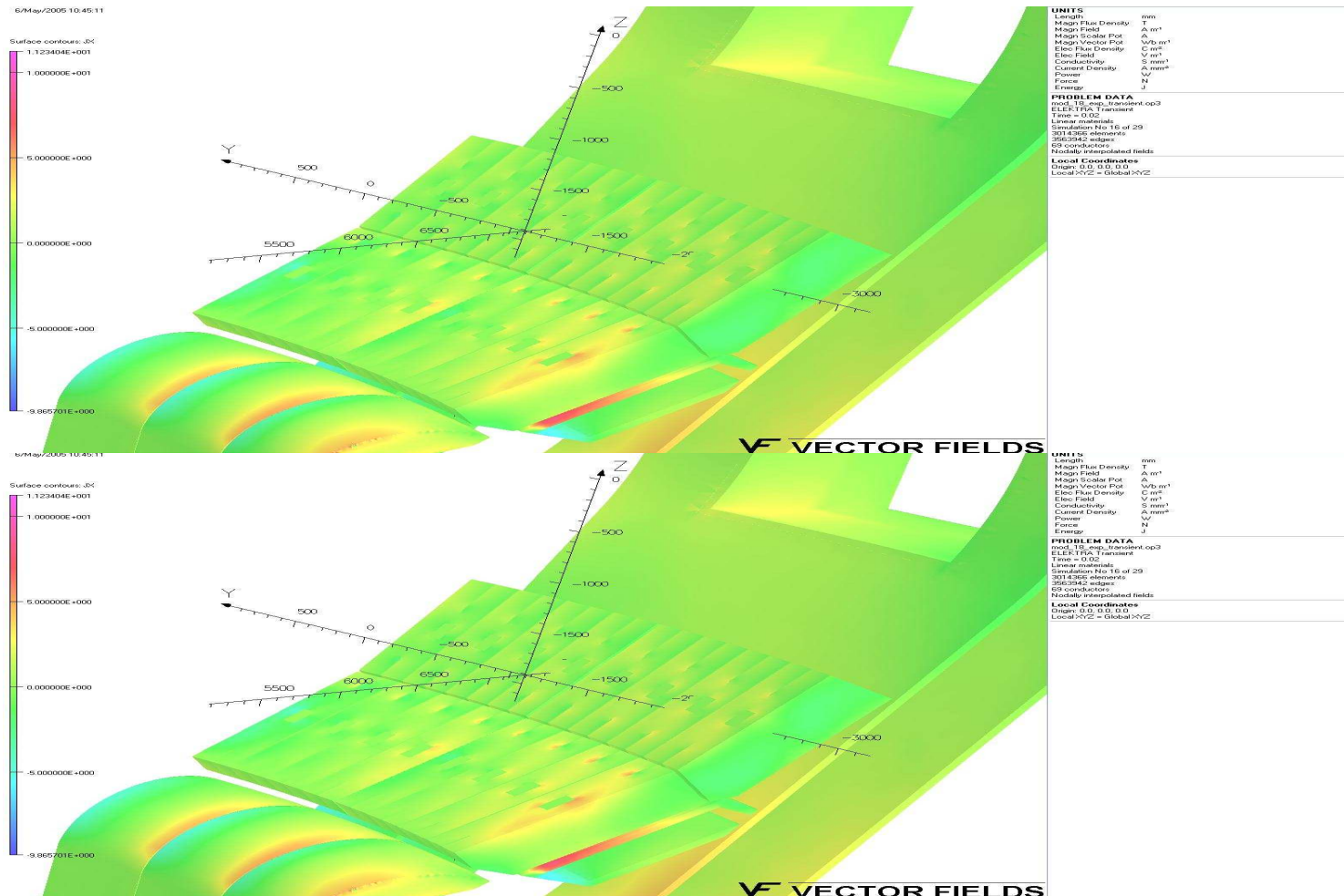
Vessel, Shield and Divertor

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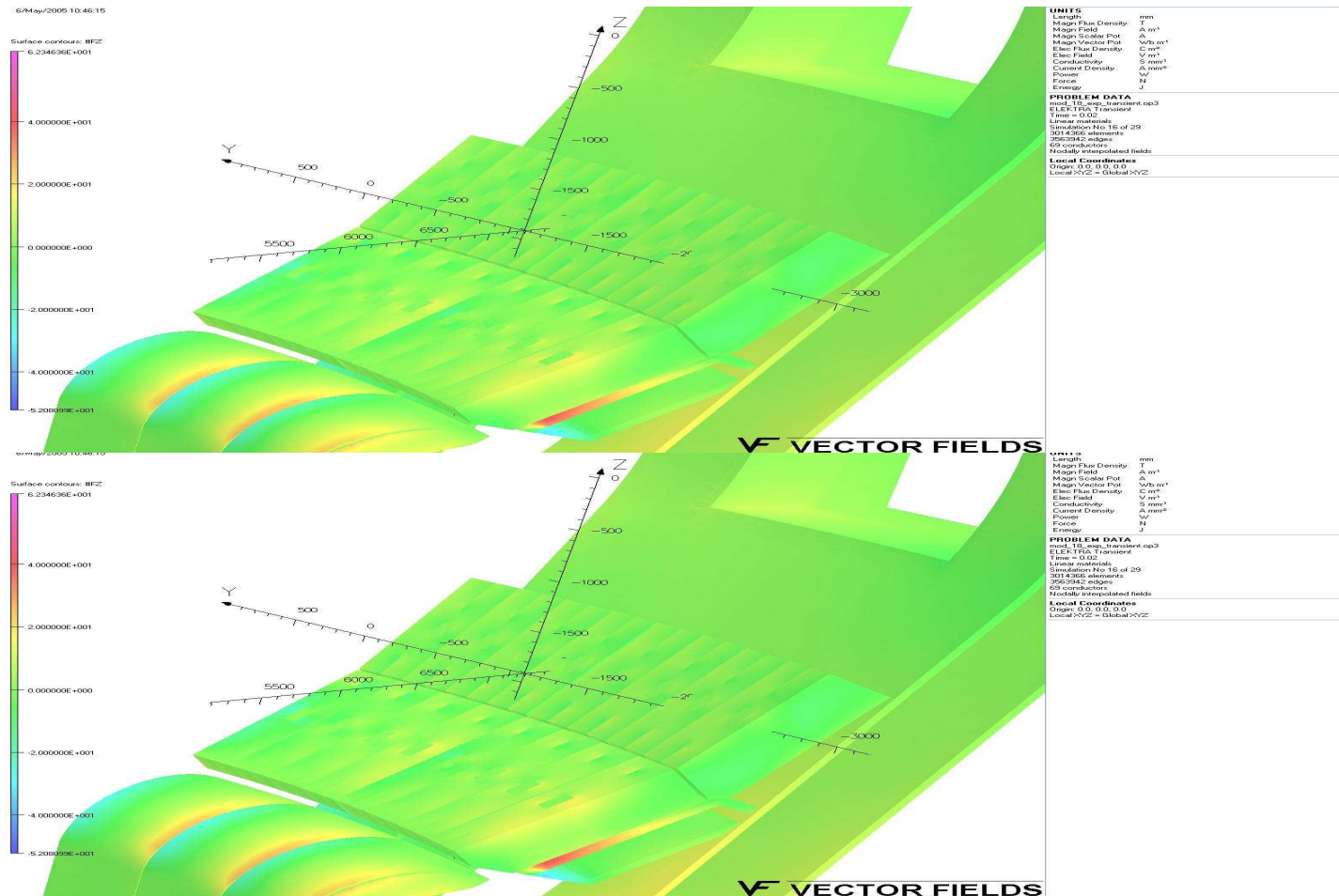


Shield Current (Preliminary)



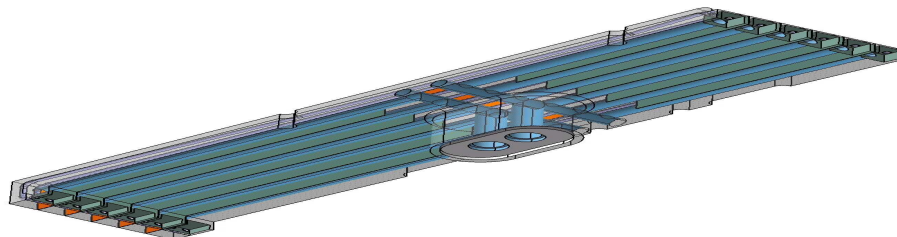
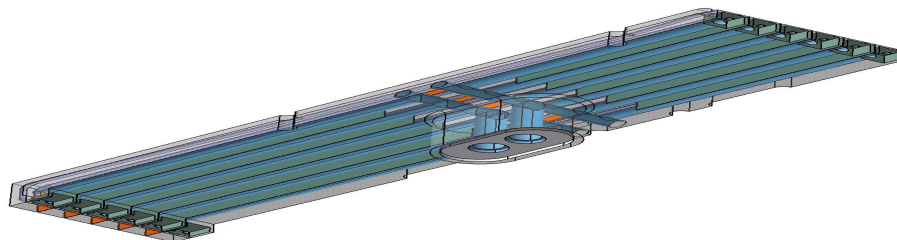
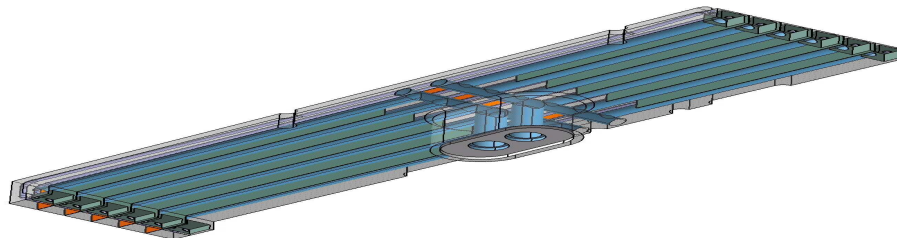


Shield Forces (Preliminary)



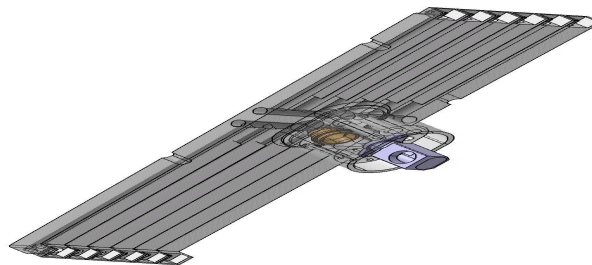
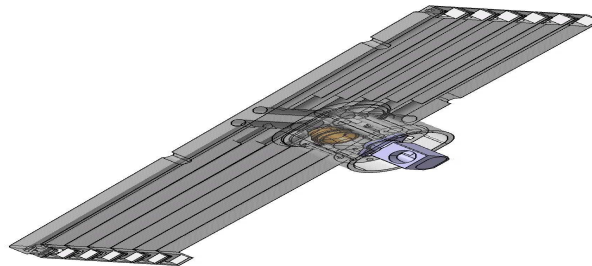
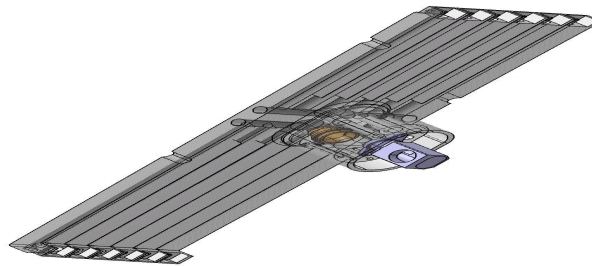


First Wall layout





First Wall layout





First Wall Thermal Analysis

- The delta T across 10 mm of Be at 50 W/cm² is 28C
- The temperature rise in the Be and Cu due to nuclear heating is negligible.
- At the normal operating point the Be has the capability of absorbing up to 18.4 J/cm² without melting.
- The temperature rise in the 316 LN is discussed earlier.



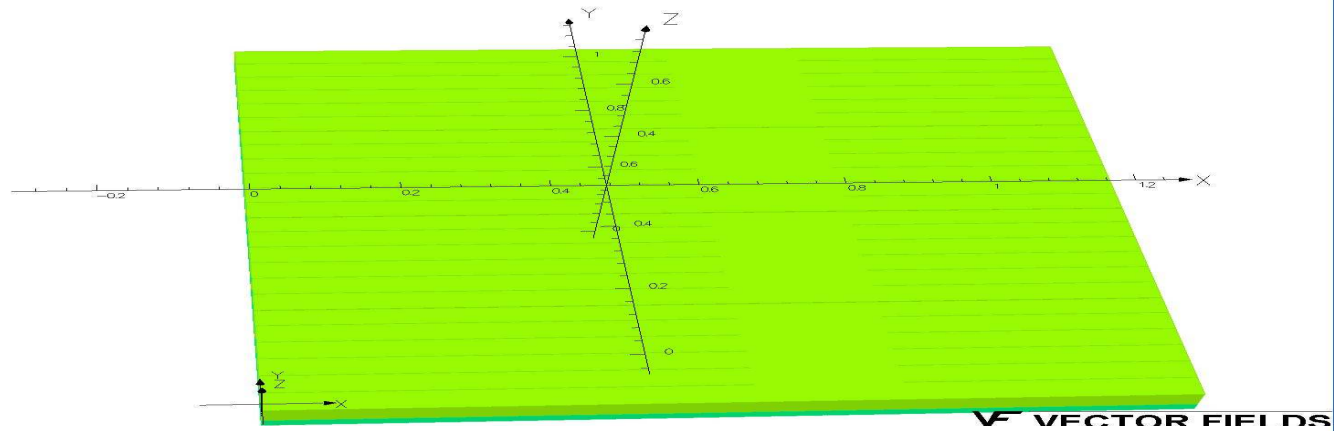
First Wall EM Analysis

- **A simplified model of the first wall was made for EM analysis while design details were worked out**
 - Rectangular only (no trapezoidal taper)
 - All fingers equal
 - No support stalk
- **EM analysis showed forces trying to twist the fingers and torque about the stalk**
- **A more realistic tapered model is being constructed**

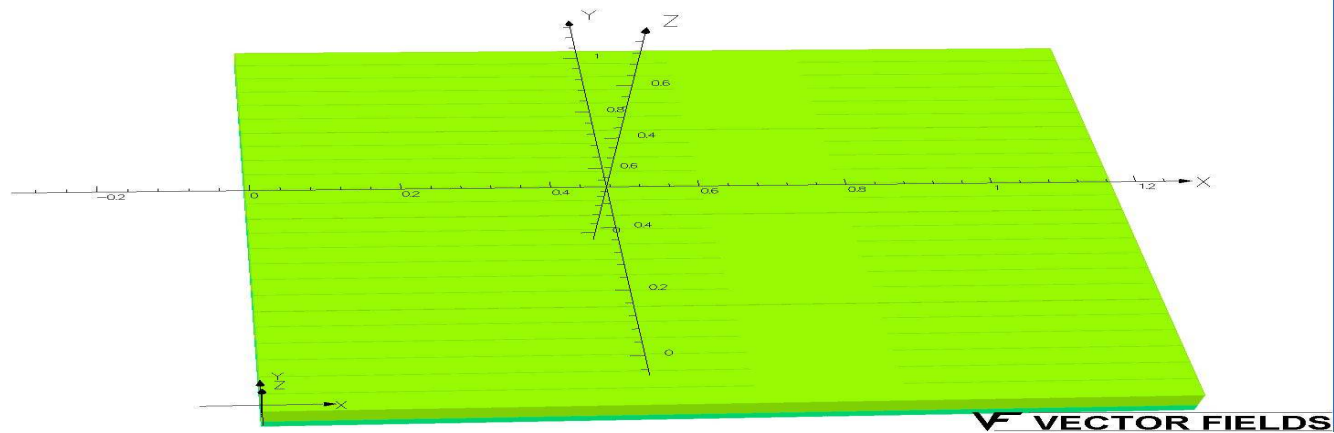


Simple FW

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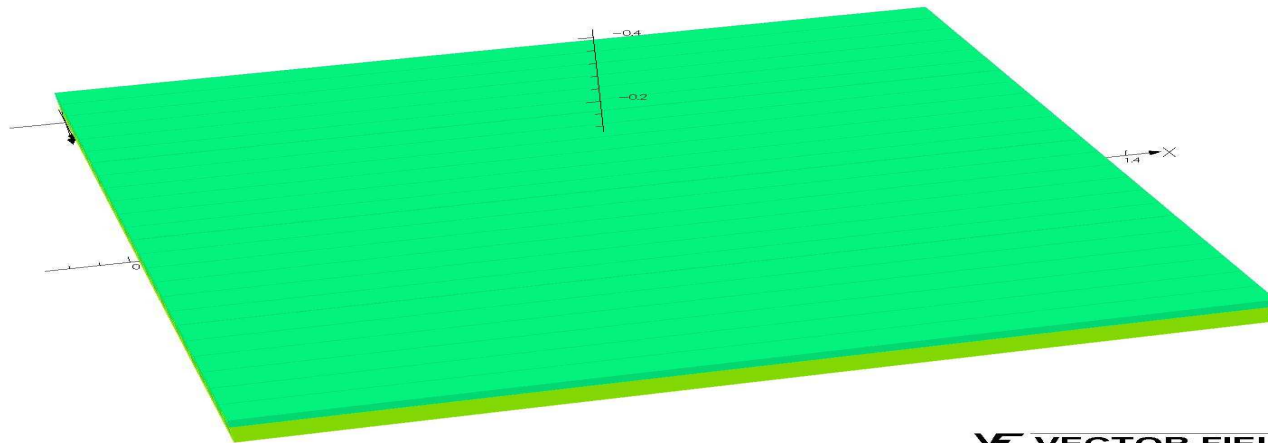
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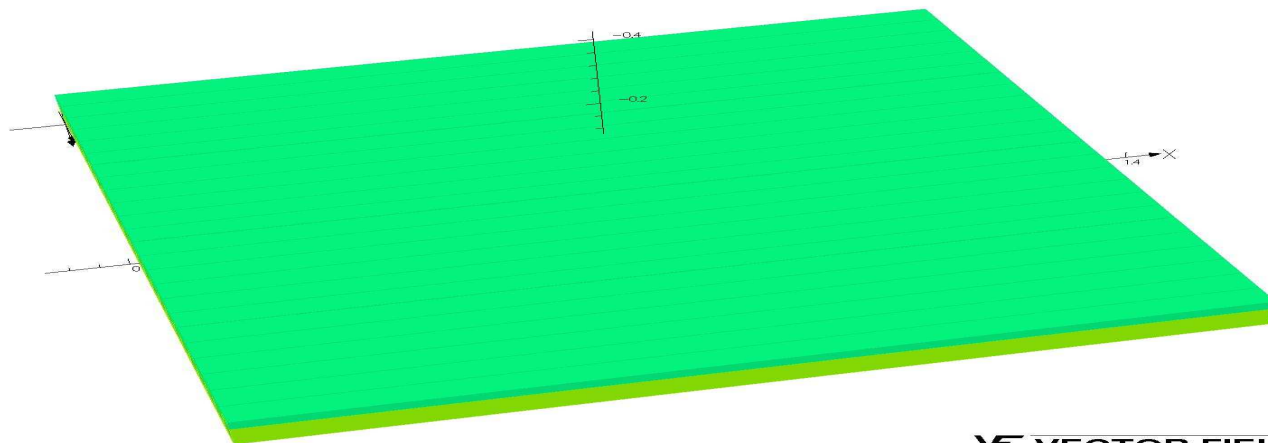
Simple FW

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\mathbf{V} VECTOR FIELDS

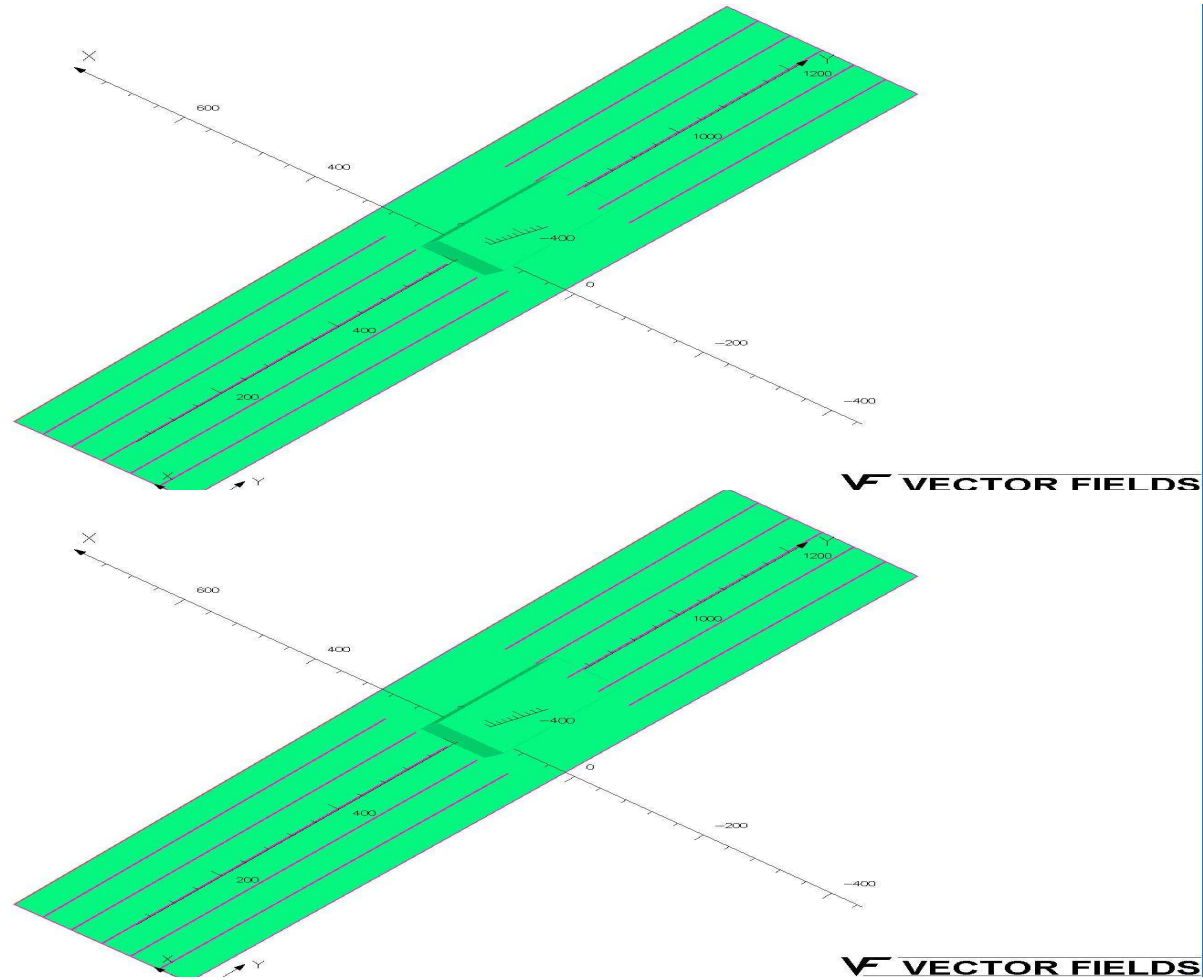


\mathbf{V} VECTOR FIELDS



Tapered FW

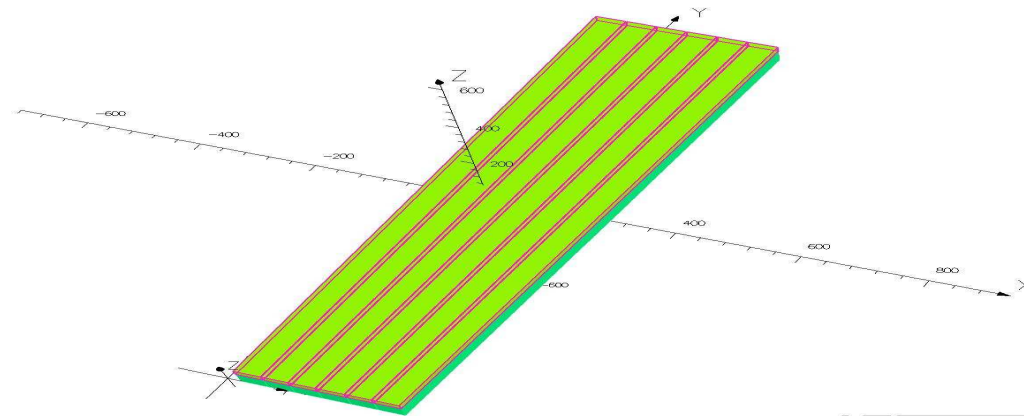
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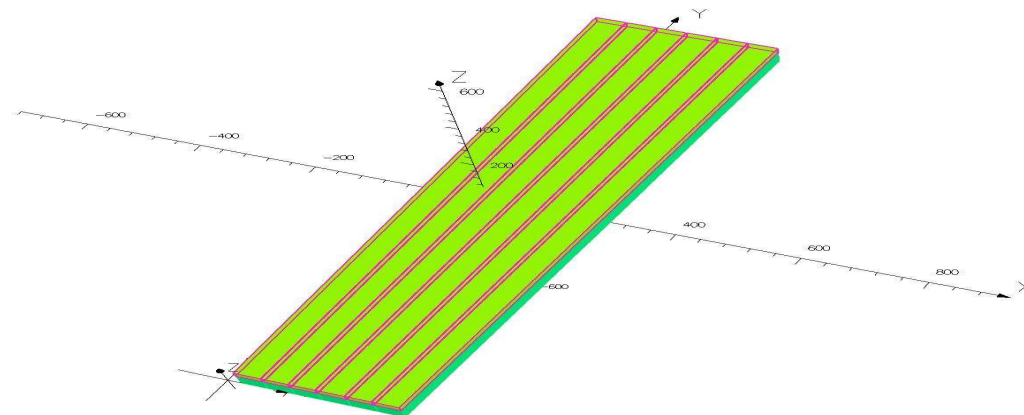
Tapered FW

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V VECTOR FIELDS

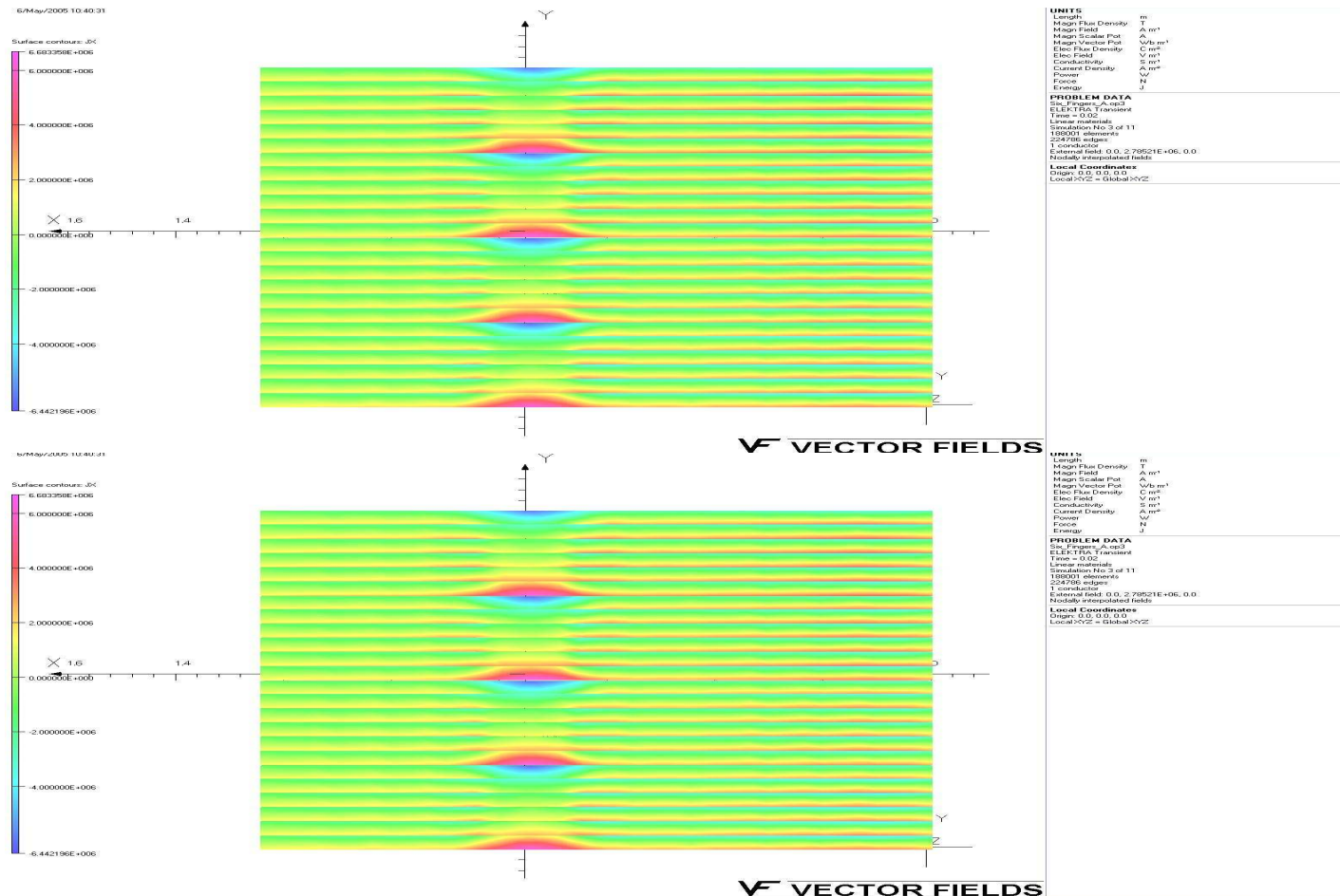
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V VECTOR FIELDS

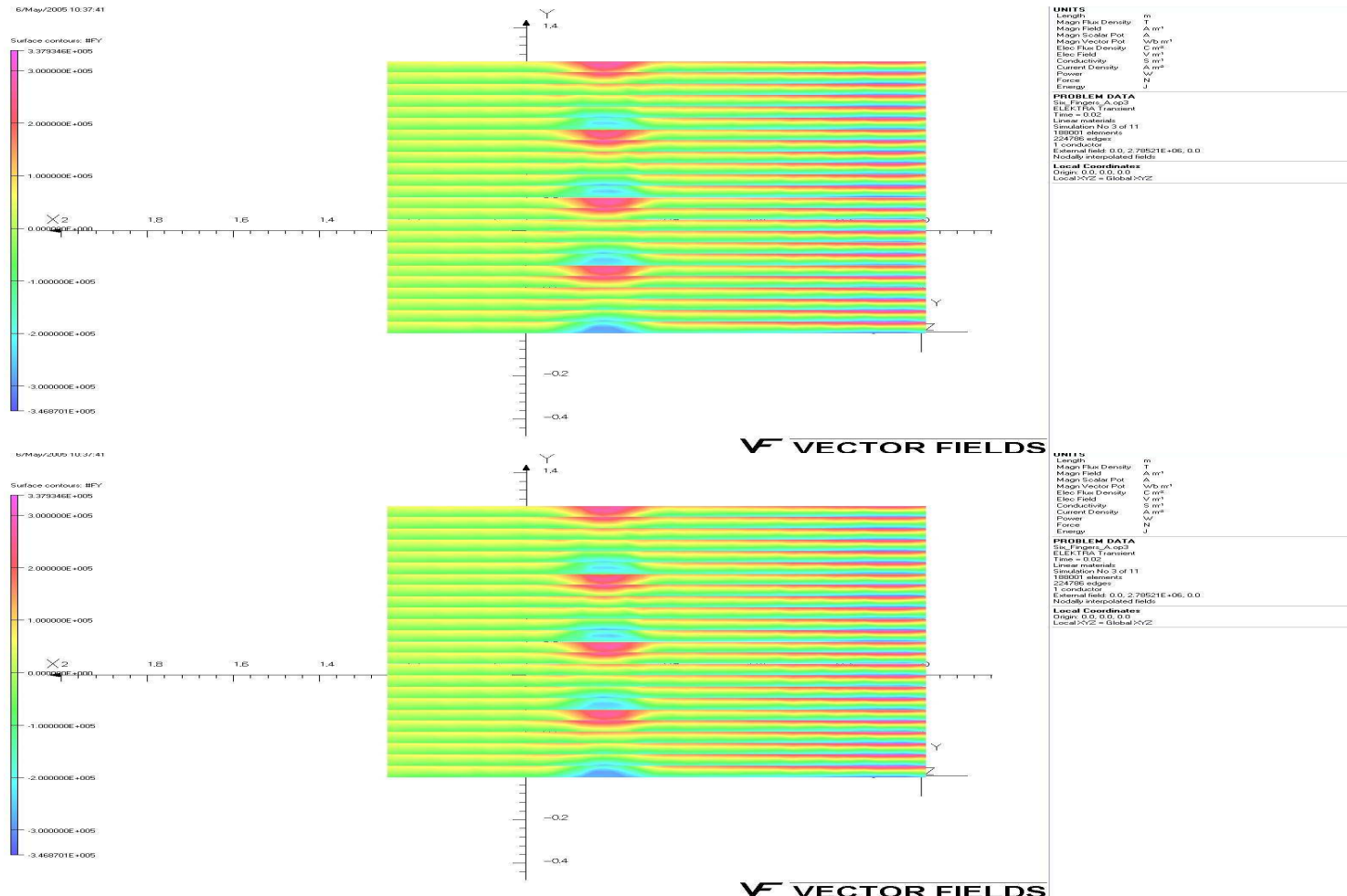


Current in the First Wall





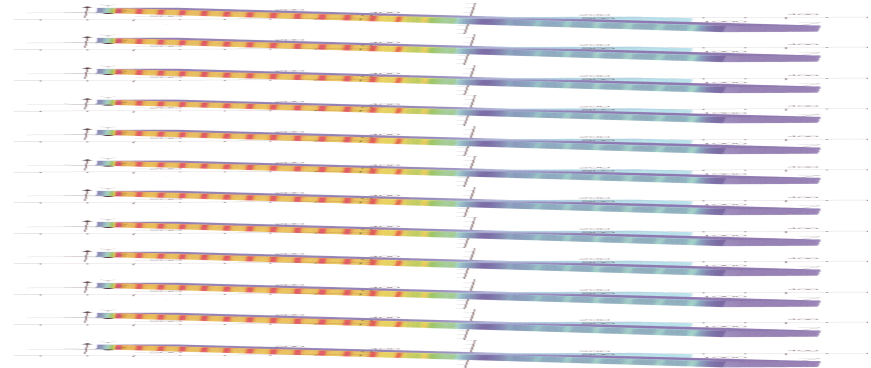
Force on the First Wall





First Wall Halo Current Simulation

- The current flow capability of OPERA has been shown to be able to simulate halo currents in the FW
- The halo currents flow in the copper layer until they get close to the stalk where the flow switches to the stalk.
- Further refinement of the model is required.





Issues to be Resolved

- **Division of the FW into panels**
 - The IT appears to be changing the FW design without complete analysis
 - Over hang of the FW beyond the shield is TBD
- **Nuclear heating of the 316 parts appears to be too large. Cause? Solution?**
- **Pressure drop in shield may be too large (redesign)**
- **R&D is needed on fabrication methods**